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# Vorwort

Das Tätigkeitsfeld des Fraunhofer-Instituts für Techno- und Wirtschaftsmathematik ITWM umfasst anwendungsnahe Grundlagenforschung, angewandte Forschung sowie Beratung und kundenspezifische Lösungen auf allen Gebieten, die für Techno- und Wirtschaftsmathematik bedeutsam sind.

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Darüber hinaus bietet die Reihe ein Forum für die Berichterstattung über die zahlreichen Kooperationsprojekte des Instituts mit Partnern aus Industrie und Wirtschaft.

Berichterstattung heißt hier Dokumentation des Transfers aktueller Ergebnisse aus mathematischer Forschungs- und Entwicklungsarbeit in industrielle Anwendungen und Softwareprodukte – und umgekehrt, denn Probleme der Praxis generieren neue interessante mathematische Fragestellungen.



Prof. Dr. Dieter Prätzel-Wolters  
Institutsleiter

Kaiserslautern, im Juni 2001



## CALCULATING INVARIANT LOADS FOR SYSTEM SIMULATION IN VEHICLE ENGINEERING

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**Abstract.** *For the numerical simulation of a mechanical multibody system (MBS), dynamical loads are needed as input data, such as a road profile. With given input quantities, the equations of motion of the system can be integrated. Output quantities for further investigations are calculated from the integration results. In this paper, we consider the corresponding inverse problem: We assume, that a dynamical system and some reference output signals are given. The general task is to derive an input signal, such that the system simulation produces the desired reference output. We present the state-of-the-art method in industrial applications, the iterative learning control method (ILC) and give an application example from automotive industry. Then, we discuss three alternative methods based on optimal control theory for differential algebraic equations (DAEs) and give an overview of their general scheme.*

## 1 INTRODUCTION

Numerical system simulation plays an important role in vehicle engineering. Virtual prototyping of mechanical systems can accelerate the development process enormously and reduces costs.

In order to simulate the motion of a multibody vehicle model, dynamic loads are needed as input data. Such load data is called *invariant*, if it is independent of the specific system under consideration. A convenient example for invariant loads is a digital road profile used for driving simulation of a vehicle.

Typically, output quantities such as wheel forces, accelerations or relative displacements in the vehicle are measured. However, those quantities are not invariant but highly dependent on the specific vehicle variant, that was used for the measurement. The general task is now to derive and calculate invariant input loads such that they can be used to simulate other vehicle variants, which may only exist as computer models. Mathematically, this leads to a control problem, see section 2 for a general formulation.

In this paper we present some approaches for dealing with this problem. State-of-the art in industrial applications is the so called *iterative learning control (ILC)* method. We give a description of that approach and an application case from automotive industry. The iterative learning control is a pure black-box method, only the input/output behaviour of the considered system is needed. This makes it also applicable to situations, for which it is hard or even impossible to get an equation, which describes the system properly, such as servo-hydraulic test-rigs in the laboratory. See [4] for a detailed description and applications. But the method lacks of precise mathematical justification, i.e. , there are no general statements about important properties like accuracy, stability, and convergence. Of course, this can be seen as a consequence of the minimal system knowledge requirement.

In contrast to the case of a servo-hydraulic test rig in the laboratory, for virtual test rigs or more generally speaking for numerical system simulation on a computer, the system is well-known as multibody system model. Therefore, it seems natural to make use of this information: our aim is to develop mathematical methods as alternatives to the ILC-approach. The general assumption is an - at least structural knowledge - of the model equations.

The methods, we are currently working on and we want to present here, are based on the theory of *optimal-control for DAEs*. The first approach is known as trajectory prescribed path control in literature, see [6]. The second method is an approach, using the calculus of variations ([5]). Both methods augment the system equation and always lead to a differential algebraic equation (DAE), which has to be solved, even if the system equation is originally an ordinary differential equation (ODE). For the numerical solution of a DAE, the (differentiation)- index is an important property, see section 2 for a definition. We give results about the index of the resulting DAE of the first two methods, see Lemmas 4.2 and 4.7.

The third alternative transfers the continuous optimal control problem to a finite-dimensional optimization problem. In literature it is known as *multiple shooting method for optimal control of DAEs* ([11], [12]).

For each approach, we give a short overview of its general scheme, and we apply it to simple test problem, an  $N$ -mass-spring-damper-system. We show, that under some assumption, the optimal control problem for this system is solvable with the best possible result, see Theorem 4.6.

## 2 The optimal control problem for dynamical systems

We formulate the optimal control problem for a general dynamical system: the *state* of the system is represented by a vector  $x(t) \in \mathbb{R}^{n_x}$ , let further  $u(t) \in \mathbb{R}^{n_u}$  denote some *input or control* quantities for the system. The dynamics of the system are described - most generally speaking - by a nonlinear *differential-algebraic equation* (DAE):

$$F(t, x(t), \dot{x}(t), u(t)) = 0, \quad t \in [0; T], \quad x(t=0) = x_0, \quad \dot{x}(t=0) = v_0, \quad (1)$$

where  $F : \mathbb{R} \times \mathbb{R}^{n_x} \times \mathbb{R}^{n_x} \times \mathbb{R}^{n_u} \rightarrow \mathbb{R}^{n_x}$  is sufficiently often differentiable and  $\frac{\partial F}{\partial x}$  is allowed to be idetically singular. If  $u$  is unknown, this equation is underdetermined.

Often, the dynamical system is given in the form of a semi-explicit DAE:

$$\begin{aligned} \dot{x}_d &= f_d(t, x_d, x_a, u) \\ 0 &= f_a(t, x_d, x_a, u) \end{aligned} \quad (2)$$

with differential variables  $x_d$  and algebraic variables  $x_a$ . The equations of motion of a (constrained) mechanical multibody system (our main interest) is a special case of such a semi-explicit DAE and has the general form:

$$\begin{aligned} \dot{q} &= v \\ M(q)\dot{v} &= f(t, q, v, u) - G^T \lambda \\ 0 &= g(q), \end{aligned} \quad (3)$$

with position coordinates  $q$ , velocities  $v$ , inputs  $u$ , and Lagrange-multipliers  $\lambda$ , i.e.,  $x = (q, v, \lambda)$ , and  $x_d = (q, v)$ ,  $x_a = \lambda$  respectively,  $G(q) := \frac{\partial g}{\partial q}$ .

We now assume, that the system outputs are given as a function of the state vector and possibly the input vector:

$$y(t) := g_{out}(x(t), u(t)) \quad (4)$$

where  $g_{out} : \mathbb{R}^{n_x} \times \mathbb{R}^{n_u} \rightarrow \mathbb{R}^{n_y}$ . We further assume, that the desired *reference outputs*, typically gained by measurement, are given as functions of time:  $y_{ref}(t) \in \mathbb{R}^{n_y}$ .

This leads to the following optimal-control problem(OCP):  
Minimize the *cost functional*

$$J[x, u] := \|y - y_{ref}\|_{L^2}^2 = \int_0^T (g_{out}(x(t), u(t)) - y_{ref}(t))^2 dt \quad (5)$$

w.r.t. to the *input/control*  $u$ , subject to Eq. (1), (2), (3) respectively. The  $L^2$ - norm could also be replaced by another suitable norm.

In general, all methods, which we describe here, require a numerical solution of a DAE, (1), (2), (3). Even, if the system equation is given as an ODE, two approaches lead to a DAE, cf. sec. 4.1 and 4.2. A well-known concept to classify DAEs is the *index*. In literature,

various definitions can be found, following [10], we introduce the *differentiation-index* to be the minimal number  $k$ , such that

$$\begin{aligned}
 F(x(t), \dot{x}(t), u(t)) &= 0 \\
 \frac{d}{dt}F(x(t), \dot{x}(t), u(t)) &= 0 \\
 &\vdots \\
 \frac{d^k}{dt^k}F(x(t), \dot{x}(t), u(t)) &= 0
 \end{aligned} \tag{6}$$

can be transformed into an ODE only by algebraic transformations. It is a well-known fact, that *higher-index* DAEs, i.e.,  $k \geq 2$  are (numerically) hard to solve.

The system equation of a constrained multibody system, eq. (3), has differentiation index 3, provided

$$GM^{-1}G^T \tag{7}$$

exists and is invertible.

A last general assumption for the rest of the paper is, that all functions are sufficiently often differentiable.

### 3 Iterative Learning Control

In this section, we describe the state-of-the-art method for industrial applications, the iterative learning control method. The method is widely used to derive drive-signals for durability test rigs in vehicle industry, cf. [4]. We give an outline of the general procedure followed by an application case from automotive industry. As stated in the introduction, the ILC does not use any information about the system equation (1), only the system's input/output behaviour is needed.

#### 3.1 The general ILC-procedure

The general ILC-procedure is divided into two steps: First, there is an identification process, in which the *frequency response function*, denoted by  $H$ , is estimated in the frequency domain. This is accomplished by a system excitation with white or pink noise as input. Secondly, one goes through a Newton-kind iteration process, in which the input is updated until the error is sufficiently small; with each input iterate  $u_i$ , the system has to be simulated in order to produce the corresponding system output,  $y_i$ , with whom in turn the input-update  $\Delta u_i$  is computed:

$$\begin{aligned}
 \Delta u_i &= H^{-1}(y_{ref} - y_i), \\
 u_{i+1} &= u_i + \Delta u_i, \\
 u_{i+1} &\xrightarrow{sim} y_{i+1}, \quad i = 0, 1, 2, \dots
 \end{aligned} \tag{8}$$

figure (1) gives an schematic overview.

For the estimation process, it is assumed, that there is a *linear, time-discrete* relationship between input and output:

$$y(k\Delta t) = H(q)u(k\Delta t) \quad k = 1, 2, \dots \tag{9}$$

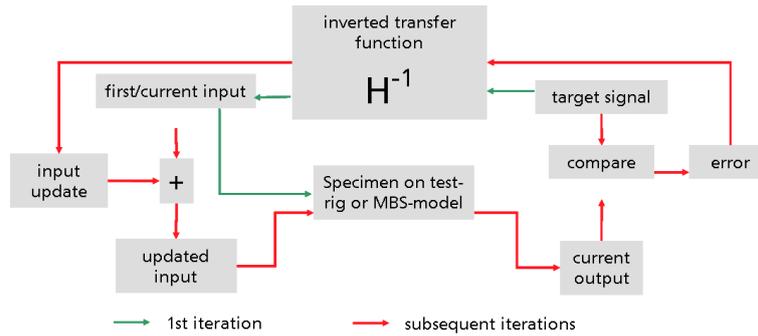


Figure 1: ILC procedure

where  $q$  is the so-called shift operator, i.e.,  $(q^{-1}u)(t) = u(t-1)$ , and  $H$  the *transfer function*:

$$H(z) := \sum_{l=1}^{\infty} g(l)z^{-l}, \quad (10)$$

with the *impulse response*  $g$ .

Then, by well-known standard routines, the frequency response function, i.e.  $H(e^{i\omega})$ , is estimated, see the book of Ljung, ([2]), for a detailed description. In the following section, we present an application example from industry, where the ILC-method has been applied successfully.

### 3.2 A Daimler truck cabin with frame on a virtual test rig

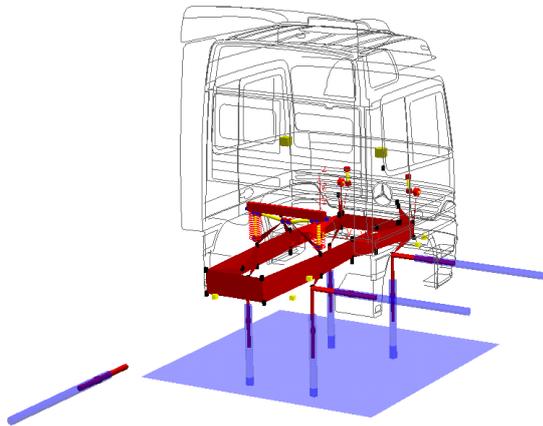


Figure 2: SIMPACK model

In a project with the Daimler AG, cf. [3], we have applied the ILC-method to a truck cabin with frame on a virtual test rig. The truck cabin, the frame and the virtual test rig have been modelled as an MBS-system in the software tool SIMPACK. The frame is mounted on the test rig, i.e., on four vertical cylinders. Additionally, there are two lateral and one longitudinal cylinders connected to the frame. Figure (2) shows the graphics of the model.

The input quantities  $u$  of that MBS model are the displacements of the seven test rig cylinders, i.e.,  $n_u = 7$ , as outputs we have defined four spring length, the connections between cabin and frame, i.e.,  $n_y = 4$ . Among others, for those spring lengths, there were reference outputs available gained by measurement. The SIMPACK model has been considered as pure black box model, which produces the corresponding spring-lengths as outputs. The ILC procedure has been performed via MATLAB-routines.

Fig. (3) shows both the measured reference output and the output, that has been generated with the calculated input, after four iteration steps.

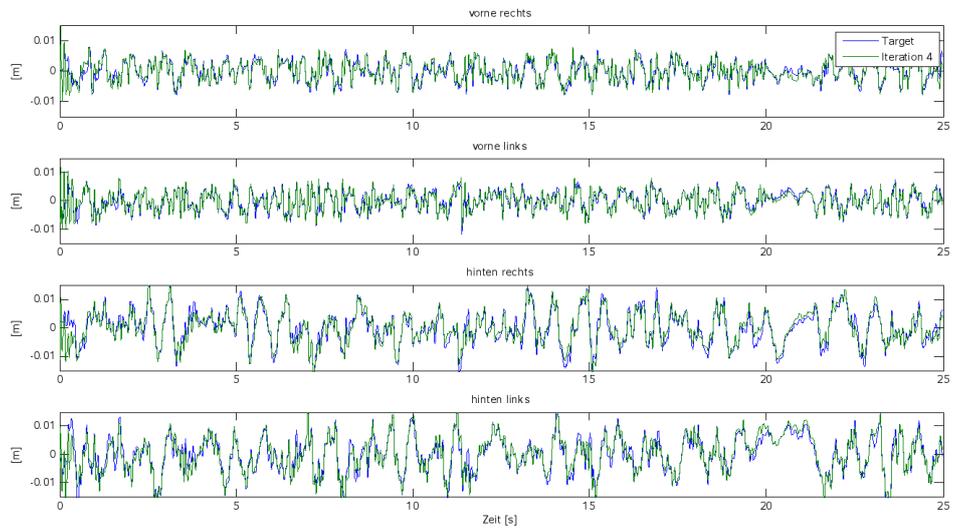


Figure 3: Reference and generated output signals

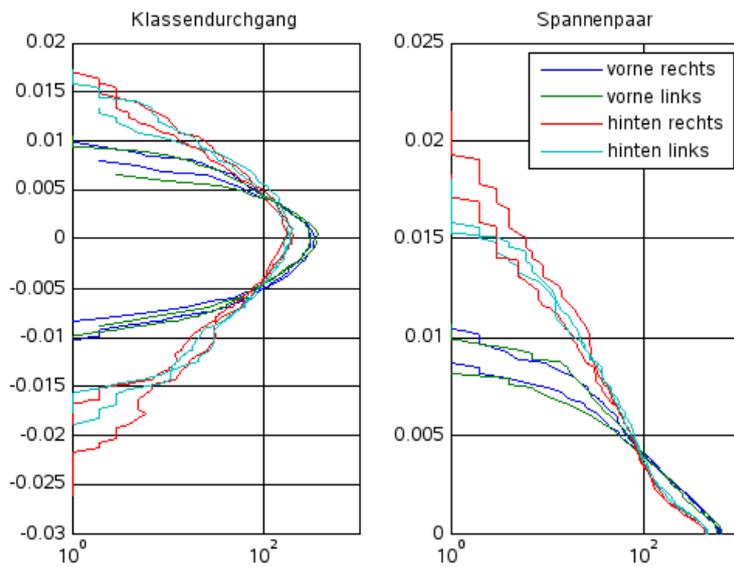


Figure 4: Left: Level crossing diagramm, right: range pair diagramm

Fig. (4) shows a level crossing diagramm to the left and a range pair diagramm to the right of the corresponding quantities. One can see, that with a relatively small number of iteration steps, the calculated output signals and the measured ones fit together very well.

#### 4 Alternative Methods

In this section, we present three alternative approaches derived from the optimal control formulation given in section 2.

In order to test the alternative methods, we have chosen a simple mechanical system as benchmark problem: a linear  $N$ -mass-spring-damper system,  $N$ -MSD, where the first body is connected to ground only by a spring. Fig. (5) shows two masses.

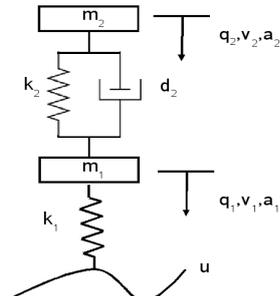


Figure 5: 2-MSD

The input of the system is the end-position of the lowest spring,  $n_u = 1$ , and the output is the motion of the highest mass, i.e., position, velocity or acceleration.

The equations of motion of that simple system are well-known and have the form:

$$\dot{x} = Ax + b \cdot u, \quad x(0) = x_0, \quad (11)$$

where  $x = (q_N, \dots, q_1, v_N, \dots, v_1)^T$ ,  $b = (0, \dots, 0, 1)^T \in \mathbb{R}^{2N}$ ,  $A \in \mathbb{R}^{2N \times 2N}$ .

In this case, the system equation is still an ODE.

##### 4.1 Trajectory prescribed path control methods

The first approach is to require the best achievable result, namely  $J[x, u] = \|y - y_{ref}\|_{L^2}^2 \equiv 0$ , in case of existence, the corresponding  $u$  is a global minimizer. This requirement is equivalent to

$$y(t) - y_{ref}(t) = g_{out}(x(t), u(t)) - y_{ref}(t) = 0 \quad \forall t \in [0; T]. \quad (12)$$

Eq. (12) can either be used to solve for one or more components of the state vector  $x$ , which can be replaced in the model equation. Then, the latter can be solved for the remaining components *and*  $u$  by a DAE-integrator. This, however, requires complete knowledge of Eq. (1) (white-box-approach). Another possibility is to simply add Eq. (12) to the model-equation (1) as a further algebraic constraint-equation, a so called *state- or path constraint*. The resulting equation is a DAE (even, if the system equation was an ODE), which is not underdetermined anymore and again, it can be solved by a DAE-integrator. This approach is known as *trajectory prescribed path control* in literature, cf. [6].

The (differentiation-)index of the resulting DAE, however, can be very high, depending on “where” the input goes into the system and which state variable appears in the output  $g_{out}$ . To make this clear, we consider the general constrained mechanical system, eq. (3) with an invertible mass matrix. Moreover, we assume that we have one input and one output,  $n_u = n_y = 1$ . We denote the  $j$ th component of the force function multiplied by the inverse mass matrix by  $f_j$ :

$$f_j(t, q, v, u) := (M(q)^{-1} f(t, q, v, u))_j \quad (13)$$

If there is an interacting force between body  $j$  and  $i$ , the corresponding force functions can be split up in

$$\begin{aligned} f_j &= f_{j,i}(q_j, q_i, v_j, v_i) + R_j \quad \text{and} \\ f_i &= f_{i,j}(q_j, q_i, v_j, v_i) + R_i = -f_{j,i}(q_j, q_i, v_j, v_i) + R_i, \end{aligned} \quad (14)$$

with  $\frac{\partial R_j}{\partial q_i, v_i} = \frac{\partial R_i}{\partial q_j, v_j} = 0$

We make the following assumption:

**Assumption 4.1.** • *The input acts only on body  $i$ , i.e.,  $\frac{\partial f_i}{\partial u} \neq 0$  and  $\frac{\partial f_k}{\partial u} = 0 \quad \forall k \neq i$*

- *We want to prescribe the acceleration of body  $j > i$ , i.e.,  $g_{out} = g_{out}(\dot{v}_j)$ .*
- *There is a connecting chain of bodies, that links bodies  $j$  and  $i$ . By this formulation, we mean: there is an interacting force between body  $j$  and  $j - 1$ , between body  $j - 1$  and  $j - 2, \dots$ , between body  $i + 1$  and  $i$  (possibly after renumeration of the bodies). Of course, the prototyping example is the  $N$ -MSD-system.*
- *For the interacting forces,  $i \leq l \leq k \leq j$ , at least one of the following conditions holds*

$$\frac{\partial f_{kl}}{\partial q_l} \neq 0 \quad (15)$$

$$\frac{\partial f_{kl}}{\partial v_l} \neq 0 \quad (16)$$

- *If equation (16) is true for all  $i \leq l \leq k \leq j$ , then the following product of Jacobians is invertible:*

$$\frac{\partial g_{out}}{\partial \dot{v}_j} \frac{\partial f_{j,j-1}}{\partial v_{j-1}} \frac{\partial f_{j-1,j-2}}{\partial v_{j-2}} \cdots \frac{\partial f_{i+1,i}}{\partial v_i} \frac{\partial f_i}{\partial u} \quad (17)$$

- *If (16) is not true for the force function  $f_{k,l}$ , then the Jacobian  $\frac{\partial f_{k,l}}{\partial v_l}$  in Eq. (17) has to be replaced by  $\frac{\partial f_{k,l}}{\partial q_l}$  and the resulting product is assumed to be invertible.*

**Lemma 4.2.** *Let Assumption 4.1 be fulfilled. Let  $N$  denote the number of bodies of the connecting chain, i.e.,  $N := j - i + 1$  and  $L$  the number of force elements between the bodies of the chain, for which eq. (16) is not true. If the system equation of the considered system has differentiation index  $D \in \{0, 1, 2, 3\}$  for given input, then the DAE which results by adding the state constraint equation  $0 = g_{out} - y_{ref}$  to eq. (3) has differentiation index*

$$\max\{D, N + L\} \quad (18)$$

*Proof.* Without loss of generality, we assume, that the original system equation is an ODE, i.e.,  $D = 0$ . We consider the case  $N = 3$  and set  $i = 1, j = i + 2 = 3$ . First we assume, that condition (16) is true for all interacting forces. For the output function we have  $g_{out} = g_{out}(\dot{v}_3) = g_{out}(f_3 = f_{32} + R_3) = \tilde{g}_{out}(q_2, v_2)$ . We differentiate the additional state constraint

equation,  $0 = g_{out} - y_{ref}$ , a first time and get (in the following, we use  $R$  as a generic symbol summarizing terms, which are not of interest):

$$\begin{aligned} 0 &= \frac{\partial g_{out}}{\partial \dot{v}_2} \frac{\partial f_{32}}{\partial v_2} \dot{v}_2 + \frac{\partial g_{out}}{\partial \dot{v}_2} \frac{\partial f_{32}}{\partial q_2} \dot{q}_2 + R = \frac{\partial g_{out}}{\partial \dot{v}_2} \frac{\partial f_{32}}{\partial v_2} f_2 + \frac{\partial g_{out}}{\partial \dot{v}_2} \frac{\partial f_{32}}{\partial q_2} v_2 + R \\ &= \frac{\partial g_{out}}{\partial \dot{v}_2} \frac{\partial f_{32}}{\partial v_2} f_{21} + \frac{\partial g_{out}}{\partial \dot{v}_2} \frac{\partial f_{32}}{\partial q_2} v_2 + R. \end{aligned} \quad (19)$$

A second differentiation yields

$$\begin{aligned} 0 &= \frac{\partial g_{out}}{\partial \dot{v}_2} \frac{\partial f_{32}}{\partial v_2} \frac{\partial f_{21}}{\partial v_1} \dot{v}_1 + \frac{\partial g_{out}}{\partial \dot{v}_2} \frac{\partial f_{32}}{\partial v_2} \frac{\partial f_{21}}{\partial q_1} \dot{q}_1 + R \\ &= \frac{\partial g_{out}}{\partial \dot{v}_2} \frac{\partial f_{32}}{\partial v_2} \frac{\partial f_{21}}{\partial v_1} f_1 + \frac{\partial g_{out}}{\partial \dot{v}_2} \frac{\partial f_{32}}{\partial v_2} \frac{\partial f_{21}}{\partial q_1} v_1 + R. \end{aligned} \quad (20)$$

And a third differentiation reveals  $\dot{u}$ :

$$0 = \frac{\partial g_{out}}{\partial \dot{v}_2} \frac{\partial f_{32}}{\partial v_2} \frac{\partial f_{21}}{\partial v_1} \frac{\partial f_1}{\partial u} \dot{u} + R. \quad (21)$$

By assumption, this equation can be resolved for  $\dot{u}$ , whence, the whole DAE has a differentiation index  $3 = 3 + 0$ .

Additionally, one can see, that for each missing damping term, i.e.,  $\frac{\partial f_{k,l}}{\partial v_l} = 0$ , one more differentiation is needed.

A simple induction argument proves the Lemma.  $\square$

**Remark 4.3.** *If we want to prescribe only the velocity of body  $j$ , i.e.,  $g_{out}$  is a function of  $v_j$ , the corresponding differentiation index naturally increases by one:  $\max\{D, N + L + 1\}$ . If  $g_{out}$  is a function only of the position  $q_j$ , the index increases by two:  $\max\{D, N + L + 2\}$*

**Remark 4.4.** *The Lemma above states, that the differentiation index of the resulting DAE of the prescribed path trajectory approach is increasing linearly with the number of “involved” bodies.*

**Remark 4.5.** *Applied to our benchmark example, an  $N$ -MSD (which is of course the prototype example of a connecting chain between two bodies), and for  $g_{out} = \dot{v}_N$ , condition (17) means*

$$d_N \cdot d_{N-1} \cdot \dots \cdot d_2 \neq 0 \quad (22)$$

*meaning, that we have dampers between every two masses. The resulting DAE has Index  $N$ . If there are  $L$  dampers missing, each corresponding  $d_l$  in the equation above has to be replaced by the corresponding spring stiffness  $k_l$ , and the DAE has index  $N + L$ . Note, that an additional damper between the first body and ground will not affect the index.*

An important property of our benchmark example is the fact, that, with the method of prescribed path trajectory, we can show, that the general task to find an input  $u$ , such that the highest mass moves as desired, i.e. follows a prescribed acceleration, velocity or position, has a solution. This solution can be written down explicitly, provided that the reference output, is smooth enough.

The crucial point is, that the system equation (11) is linear. We can transform the corresponding DAE, the system equation and the state constraint equation  $g_{out}(q_N, v_N) - y_{ref}(t) = 0$ , in the following standard form:

$$E\dot{\tilde{x}} = \tilde{A}\tilde{x} + f(t), \quad (23)$$

with  $\tilde{x} = (x, u)^T \in \mathbb{R}^{2N+1}$ , a singular matrix  $E$  and  $f(t) = (0, \dots, 0, -y_{ref}(t))^T \in \mathbb{R}^{2N+1}$ .

To guarantee solvability of that DAE, we still have to require the further condition, that the matrix pair  $(E, \tilde{A})$  is regular, i.e., there is a  $\lambda \in \mathbb{C}$  such that  $\det(\tilde{A} - \lambda E) \neq 0$ .

**Theorem 4.6.** *If  $(E, \tilde{A})$  is regular and the reference output  $f$  is smooth enough, then DAE (23) is solvable. The solution can be written down explicitly. The solution-algorithm, given in the proof, reveals directly the index of the DAE.*

*As a consequence, the optimal-control problem, we consider for the  $N$ -MSD has a solution, that fulfills  $J[x, u] \equiv 0$ .*

*Proof.* The pair  $(E, \tilde{A})$  can be transformed to the Weierstraß-canonical form, i.e., there are regular matrices  $P, Q$ , such that

$$PEQ = \begin{pmatrix} \tilde{N} & \\ & \mathbb{1} \end{pmatrix} \quad P\tilde{A}Q = \begin{pmatrix} \mathbb{1} & \\ & J \end{pmatrix} \quad (24)$$

with a nilpotent matrix  $\tilde{N}$  and a matrix  $J$  in Jordan canonical form.

With the obvious coordinate transformation and a multiplication by  $P$ , Eq. (23) splits up into the two independent equations

$$\begin{aligned} \tilde{N}\dot{\bar{x}}_1 &= \bar{x}_1 + (Pf)_1 \\ \dot{\bar{x}}_2 &= J\bar{x}_2 + (Pf)_2 \end{aligned} \quad (25)$$

The solution is

$$\begin{aligned} \bar{x}_1(t) &= - \sum_{\nu=0}^i \tilde{N}^\nu (Pf)_1^{(\nu)}(t), \\ \bar{x}_2(t) &= \int_0^t e^{J(t-s)} (Pf)_2(s) ds \end{aligned} \quad (26)$$

where  $i$  is the index of nilpotency of the matrix  $\tilde{N}$ , which is obviously also the index of the DAE. See [8] for details.  $\square$

For our test-problem, however, we have followed both ways. the following figures show a comparison. For this test, we have chosen a 3-MSD system, we have prescribed the acceleration of the highest mass to be sine-function, i.e., the state-constraint equation added to the system equation is  $0 = g_{out}(\dot{v}_3) - y_{ref}(t) = \dot{v}_3 - \sin(t)$ . There are no dampers missing, so, according to Lemma (4.2), the index of the resulting DAE is  $1 + 2 = 3$ , therefore, it can be solved numerically by the DAE-Integrator RADAU5, see [7], without any index reduction.

The error-tolerances of RADAU5 were set to  $10^{-4}$ , both relative and absolute, RADAU5 has taken 118 time steps to solve this simple Index-3-problem.

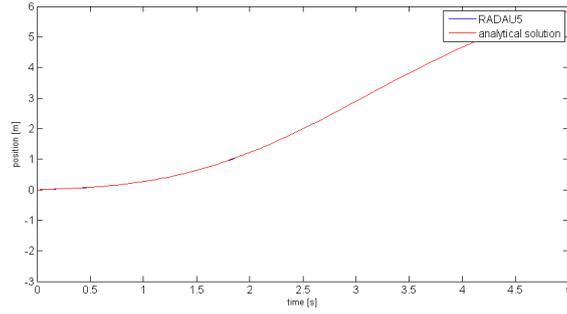


Figure 6: Input

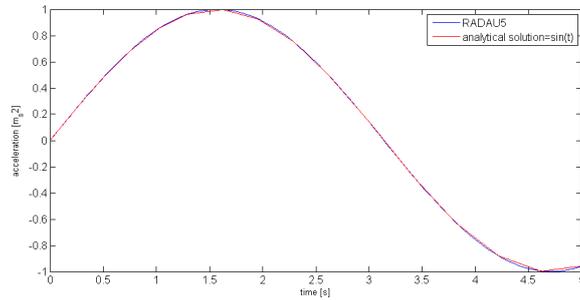


Figure 7: Output, acceleration of the highest mass

## 4.2 Variational Method

The next approach, we want to discuss here, is a variational approach, in literature also often called indirect optimization. For a detailed overview, see [5], [9].

Recall, that our general task is to minimize the cost functional,

$$J[x, u] := \|y - y_{ref}\|_{L^2}^2 = \int_0^T (g_{out}(x(t), u(t)) - y_{ref}(t))^2 dt, \quad (27)$$

subject to the equation, which describes the dynamics for the multibody system. For this section, we assume, that the system equation is an ODE of the form

$$\dot{x} = f(t, x, u), \quad x(0) = x_0, \quad (28)$$

again with  $x = (q, v)^T$ . The idea of the variational approach is to derive a necessary condition for  $u$  to be a minimizer of (27). We briefly sketch the well-known argumentation: we consider small perturbations of  $u$ :  $u + \varepsilon \delta u$ . If  $x$  is a solution of (28) to  $u$ , the solution corresponding to the perturbed input is of the form  $x + \varepsilon \delta x + \mathcal{O}(\varepsilon^2)$  and therefore

$$\dot{\delta x} = f_x \delta x + f_u \delta u. \quad (29)$$

Linearization of the cost functional yields

$$J[u + \varepsilon \delta u] - J[u] = \varepsilon \int_0^T (\varphi_x \delta x + \varphi_u \delta u) dt + \mathcal{O}(\varepsilon^2), \quad (30)$$

we have set  $\varphi(t, x, u) := g_{out}(x(t), u(t)) - y_{ref}(t)$ . Hence, a necessary condition for  $u$  to be a minimizer is

$$\int_0^T (\varphi_x \delta x + \varphi_u \delta u) dt = 0. \quad (31)$$

It is easy to show, that this is equivalent to

$$\int_0^T (\mu^T f_u + \varphi_u) \delta u dt = 0, \quad (32)$$

provided, that the so called adjoint variable  $\mu$  fulfills

$$\dot{\mu} = -f_x^T \mu - \varphi_x^T, \quad \mu(T) = 0. \quad (33)$$

To summarize, a necessary condition for  $u$  to be a minimizer is fullfilling the DAE-system:

$$\begin{aligned} \dot{x} &= f(t, x, u), & x(0) &= x_0, \\ \dot{\mu} &= -f_x^T \mu - \varphi_x^T, & \mu(T) &= 0, \\ 0 &= \mu^T f_u + \varphi_u. \end{aligned} \quad (34)$$

For a detailed discussion, see [5].

Eq. (34) is a mixed boundary value DAE-problem (of possibly high index). Hence, it is numerically hard to solve, e.g., one can apply shooting methods, that in turn require derivatives with respect to the end value  $\mu(T)$ . These derivatives can be obtained by a finite differences approximation, by integrating the corresponding sensitivity DAE or by algorithmic differentiation.

We consider our benchmark problem, the  $N$ -MSD, see Eq. (11). Again, we want to prescribe the motion of the  $N$ -th mass

The variational equations (34) for this problem read as follows:

$$\dot{x} = Ax + bu, \quad x(0) = x_0, \quad (35)$$

$$\dot{\mu} = -A^T \mu - \varphi_x^T, \quad \mu(T) = 0, \quad (36)$$

$$0 = \mu^T b = \mu_{2N} k_1. \quad (37)$$

For the different output possibilities, we have:

$$\begin{aligned} \text{acceleration: } \varphi(t, x, u) &= (-k_N(x_N - x_{N-1}) - d_N(v_N - v_{N-1}) - y_{ref}(t))^2, \\ \text{velocity: } \varphi(t, x, u) &= (v_N - y_{ref}(t))^2, \\ \text{position: } \varphi(t, x, u) &= (x_N - y_{ref}(t))^2, \end{aligned} \quad (38)$$

whence, for the gradient:

$$\begin{aligned} \text{acceleration: } \varphi_x^T &= (-k_N, k_N, 0, \dots, 0, -d_N, d_N, 0, \dots, 0)^T \\ &\quad \cdot 2(-k_N(x_N - x_{N-1}) - d_N(v_N - v_{N-1}) - y_{ref}(t)), \\ \text{velocity: } \varphi_x^T &= (0, \dots, 0, 2(v_N - y_{ref}(t)), 0, \dots, 0)^T, \\ \text{position: } \varphi_x^T &= (2(x_N - y_{ref}(t)), 0, \dots, 0)^T. \end{aligned} \quad (39)$$

For the index of the DAE system (35)-(37), we have a similar result as for the index for the resultig DAE of the previous method, it grows linearly with the number of bodies:



### 4.3 Direct Optimization - a multiple shooting method

The last approach, we want to present here, is based on a direct optimization of the optimal control problem (5), it is transformed to a finite-dimensional nonlinear programming problem, see [11], [12].

Here, we assume, that the system equation is a DAE in semi-explicit form:

$$\begin{aligned} \dot{x}_d &= f_d(t, x_d, x_a, u), \\ 0 &= f_a(x_d, x_a, u), \end{aligned} \quad (48)$$

with differential variables  $x_d$  and algebraic variables  $x_a$ .

We give a brief overview of the discretization procedure: First, we introduce a control grid,

$$\pi_u := \{t_1, \dots, t_M\} \subset [0; T] \quad t_1 = 0, t_M = T, \quad (49)$$

on which the input  $u$  is approximated by splines. E.g., one can think of a piecewise constant or linear approximation on each subinterval  $[t_i; t_{i+1}]$ . Let  $c_1, \dots, c_{\tilde{M}}$  denote the corresponding spline coefficients.

The next step is to introduce a state grid

$$\pi_x := \{\bar{t}_1, \dots, \bar{t}_L\} \subset [0; T], \quad \bar{t}_1 = 0, \bar{t}_L = T. \quad (50)$$

On each subinterval  $[\bar{t}_j; \bar{t}_{j+1}]$ , the system equation is solved numerically by a suitable integrator. An important condition is, that we have consistent ‘‘initial’’ values  $x^j = (x_d^j, x_a^j)$  at each state grid point. Let

$$x_{app}^j = x_{app}^j(t; x^j, c) \quad (51)$$

denote the approximate solution on  $[\bar{t}_j; \bar{t}_{j+1}]$ , depending on the spline coefficients, which will appear later as a part of the variable to be changed in the optimization process.

The last task is to discretize the cost functional

$$J[x, u] := \int_0^T \varphi(t, x, u) dt. \quad (52)$$

To this end, there are mainly two possible ways. The first one is to approximate the integral by a finite sum, possibly on a third time grid  $\pi_J := \{\tilde{t}_1, \dots, \tilde{t}_K\} \supset \pi_x$ :

$$J[x, u] := \int_0^T \varphi(t, x, u) dt \approx \tilde{J}[x, u] := \sum_{i=0}^K h_i \varphi(\tilde{t}_i, x(\tilde{t}_i), u(\tilde{t}_i)) \quad (53)$$

with suitable weighting factors  $h_i$ .

To explain the second way, we remark, that the form of our optimal control problem - with the cost functional being an integral - is said to be in *Lagrange form* in literature. It can easily be transformed into a problem in so called *Mayer form*, in which the cost functional is only function of the state variable at the end time:  $J[x, u] = \Phi(x(T))$ . Of course, such a cost functional has not to be discretized anymore. The transformation is accomplished by introducing an additional state variable  $x_0$  and an additional differential equation

$$\dot{x}_0 = \varphi(t, x, u), \quad x_0(0) = 0. \quad (54)$$

Adding this differential equation to the system equation and setting

$$\tilde{J}[x, u] := x_0(T), \quad (55)$$

we arrive at an optimal control problem in Mayer form, which is equivalent to our old problem. Now, we are able to state the discretized, finite-dimensional optimal control problem:

$$\begin{aligned} \text{minimize} \quad & \tilde{J}[x, u] \\ \text{w.r.t.} \quad & \zeta := (x_d^1, \dots, x_d^L, c_1, \dots, c_{\tilde{M}}) \\ \text{s.t.} \quad & x_{d,app}^1(\tilde{t}_2; x_d^1, c) = x_d^2 \\ & \vdots \\ & x_{d,app}^{L-1}(\tilde{t}_{L-1}; x_d^{L-1}, c) = x_d^L \end{aligned} \quad (56)$$

Note, that the optimization variable  $\zeta$  only depends on state grid initial values of the differential variable. To be consistent, the initial value of the algebraic variable is locally uniquely determined. The last constraint equations of (56) assure, that the differential part of the approximate solution is continuous.

The whole method is called *direct single shooting method*, if  $L = 1$ , and *direct multiple shooting method* otherwise. The dimension of the optimization variable  $\zeta$  is finite, but can be very high, depending on the length of the complete time interval to be considered and on the length of the discretization time grids. Suitable numerical solution methods for such nonlinear programming problems are sequential quadratic programming methods (SQP), see [14]. Those methods, however, use the gradient of the objective function and the Jacobian of the constraints, i.e., as in the variational approach, a sensitivity analysis of the system equation is often necessary.

To reduce the dimension of the optimization variable, so called *moving horizon techniques* are proposed in literature, see [13]. The main idea is to consider short sections of the complete time interval  $[0; T]$  and solve local optimal control problems of smaller dimension. The local solutions have to be combined by suitable transient conditions.

We have applied this approach to our benchmark problem, this time a 2-MSD, where the output was the displacement of the highest mass and the reference output was a sine signal again. The following figures show the results.

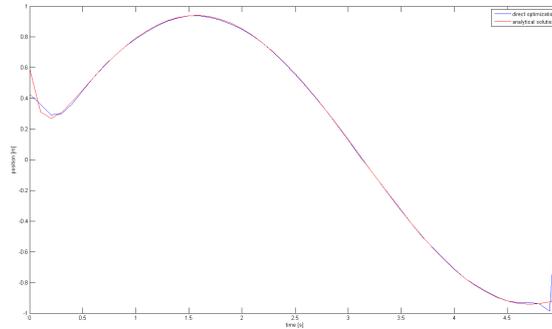


Figure 8: Calculated input and the exact solution

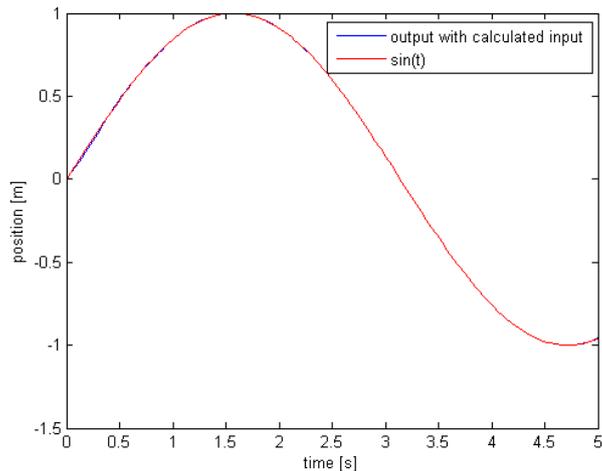


Figure 9: Calculated output and the exact solution, displacement of the highest mass

#### 4.4 Comparison

We have presented three mathematically well-defined approaches for dealing with the optimal control problem described in the introduction. All three methods work very well for our benchmark system, a  $N$ -mass-spring-damper system, with small  $N$ .

Both the trajectory prescribed path control method and the variational approach augment the system equation of the considered dynamical system and always lead to a DAE. The two approaches, however, can suffer from a high differentiation index of the resulting DAE. As we have shown in the Lemmas 4.2, 4.7, without any modifications, for both methods, the differentiation index is increasing with  $\mathcal{O}(N)$ , where  $N$  is the number of involved bodies. It is well-known, that this can lead to severe numerical difficulties or even to a numerical unsolvability of the DAE. The integrator RADAU5 can solve DAEs in semi-explicit form up to index 3. Concerning the variational approach, we have the additional problem, that the underlying DAE is a mixed boundary value problem, so, e.g., a shooting method has to be applied, which in turn requires derivatives, i.e., in this case, Hessians of the right-hand side of the system equation. Note, that one needs Jacobians of the right-hand-side of the system equation only to set up the variational equations, eq. (34).

The last approach, the direct optimization, has no such index problems as the previous ones. Here, the system equation is not affected and the differentiation index remains unchanged. The resulting optimization problem can be solved with a suitable large-scale algorithm, if its dimension is not too high. Otherwise, other techniques, such as moving horizon, are necessary. Additionally, optimization methods usually need gradients of the object function and Jacobians of the constraints, i.e., in this case Jacobians of the right-hand side of the system equation.

As information about the considered dynamical system, the three methods merely require a structural knowledge and right-hand-side evaluations as well as evaluations of the right-hand-side-Jacobians and -Hessians respectively. Hence, an application in connection with a commercial MBS tool could be possible. However, if an index reduction has to be performed for

one of the first two methods, surely more information about the system equation is necessary. Concerning the needed information about the system equation, one could tax the first two methods as *grey-box* methods, whereas the third approach is “*dark-grey*”, since only the integration results of the system equation and the corresponding sensitivity equation are needed.

## 5 Conclusion

In this paper, we have presented the problem of calculating invariant loads for the simulation of dynamical systems in vehicle engineering. Mathematically, the problem is an optimal control problem. We have described the state-of-the-art solution, the iterative learning control, and have given an application example from the automotive industry, for which the iterative learning control has been applied successfully. However, this method has many drawbacks and does not converge for general nonlinear systems. Therefore, we have presented three alternative approaches, based on the optimal control theory for DAEs. We have successfully applied those methods to simple benchmarks and investigated some of the problems and numerical difficulties occurring there. Currently, we are working on the refinement and implementation of the described methods.

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Keywords: flexible multibody dynamics, large deformations, finite rotations, constrained mechanical systems, structural dynamics  
(20 pages, 2009)

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Keywords: special Cosserat rods, Lagrangian mechanics, Noether's theorem, discrete mechanics, frame-indifference, holonomic constraints  
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Keywords: iterative learning control, optimal control theory, differential algebraic equations(DAEs)  
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